Set of Components/Component	-	Three-Way Control Valve Type Z3 / BR13 with Diaphragm Multi-Spring Pneumatic Actuator (P/R & P1/R1)									
Control Valve Z3 / BR13	SIL-Report,	SIL-Report, Report No. B160302, Version 1.0, (all variants)									
Pneumatic Actuator P/R & P1/R1		SIL-Report, Report No. B130392, Version 1.0, (type P/R & P1/R1, variant single + tandem, spring range 17, without handwheel)									
Manufacturer	Zaklady Aut	Zaklady Automatyki "POLNA" S.A.									
Component Type	Type A (Ref	Type A (Ref. IEC 61508-29									
Mode of Operation	Low demand	Low demand operation									
Safety Function, SF1	Actuator close	Actuator closes valve by spring force. Valve closes vertical outlet (1) and opens horizontal flow within specified safety time ("valve closing").									
Safe State, SS1	Vertical outlet flow opened w	Vertical outlet (1) of the valve closed with specified leakage rate, horizontal flow opened with specified mass flow rate (state: "valve closed"). Actuator holds valve in safe position with specified force.									
Safety Function, SF2	Actuator open shutoff horizor	Actuator opens valve by spring force. Valve opens vertical outlet (1) and shutoff horizontal flow within specified safety time ("valve opening").									
Safe State, SS2	flow shutoff wi	Vertical outlet of the valve (1) opened with specified mass flow rate, horizontal flow shutoff with specified leakage rate (state: "valve opened"). Actuator holds valve in safe position with specified force. (1)									
	Failure	Rates [f	ailure/10 ⁹ h	rs = FIT]							
Failure Rate Distribution	λtotal	λsafe	λ dangerous det	ected λdange	rous undetected	λdon't care	SFF [%				
Control Valve Z3 / BR13	38	0	27		11	41	71				
Diaphragm Actuator P/R & P1/R1	3,135	2,950	57		128*	1	96				
Control Valve Z3 / BR13 with Diaphragm Actuator P/R & P1/R1	3,173	2,950	84		139	42	96				
* D	esign of actuator toler		•								
Arabitaatura	Specificatio	1	-			and the second states of the s					
Architecture Hardware Fault Tolerance HFT	1001 0	Due to HET_0, one foilure has impact on the sofety function of a single set of									
MTTR / MRT	32 h / 8 h	components/component of the analyzed type. MTTR is the time required to detect and for repair of the component in case of failure. MTR is the									
Diagnostic Coverage (DC)	38 %	In case of mis	ssing automatic o	liagnosis: DC = 0 %	. In case of implen						
Diagnostic Test	PST	Diagnostic test used to detect dangerous failures during operation. PST: Partial Stroke Test, valves with actuator in open/close application is moved out of activated									
		Max. diagnostic test interval to perform online diagnostics to detect potential datual varie position. Max. diagnostic test interval to perform online diagnostics to detect potential dangerous failures during operation amounts to 24 h. Deviating diagnostic test interval must be considered in pfd- calculation, by deviating MTTR.									
Diagnostic Test Interval	24 h		y deviating MTT		$β_{int} = 5\%$ Beta factor, which has to be considered if the components/component are used in safety relevant architectures with a HFT ≥ 1. Detailed beta factor has to be calculated for each individual application The beta factor depends on the exact architecture where the components/component is used in. Se IEC 61508-6, table D.5 how to calculate beta factor.						
Diagnostic Test Interval Beta Factor	β _{int} = 5%	calculation, b Beta factor, w architectures The beta fact	which has to be c with a HFT ≥ 1. I for depends on th	onsidered if the con Detailed beta factor e exact architecture	has to be calculate where the compo	ed for each individ					
Beta Factor	$β_{int} = 5\%$ $β_{Dint} = 2\%$ n of SIL Capa	calculation, b Beta factor, w architectures The beta fact IEC 61508-6, ability (ex	which has to be co with a HFT \geq 1.1 for depends on th table D.5 how to camples co	Desidered if the com Detailed beta factor e exact architecture calculate beta fact	has to be calculate where the compo or.	ed for each indivio nents/component					
Beta Factor Verification	$β_{int} = 5\%$ $β_{Dint} = 2\%$ n of SIL Capa	calculation, b Beta factor, w architectures The beta fact IEC 61508-6, ability (ex	which has to be converted with a HFT \ge 1. If the total of the total with a HFT \ge 1. If total of the total of total of the total of t	Desidered if the com Detailed beta factor e exact architecture calculate beta fact	has to be calculate where the compo or.	ed for each indivio nents/component	is used in. Se				
Beta Factor	$\beta_{int} = 5\%$ $\beta_{Dint} = 2\%$	calculation, b Beta factor, w architectures The beta fact IEC 61508-6, ability (ex	which has to be c with a HFT ≥ 1. I for depends on th table D.5 how to camples co page/backside of	exact architecture calculate beta factor calculate beta factor calculate beta factor considering d this page) 2 years	has to be calculate where the compo or.	ed for each indivio nents/component St)	is used in. See				
Beta Factor Verification Proof Test Interval	$\beta_{int} = 5\%$ $\beta_{Dint} = 2\%$ of SIL Capa (see control (see control	calculation, b Beta factor, w architectures The beta fact IEC 61508-6, ability (ex	which has to be c with a HFT ≥ 1.1 or depends on th table D.5 how to camples cc page/backside of 1 year	exact architecture calculate beta factor calculate beta factor calculate beta factor considering d this page) 2 years	has to be calculate where the compo or. iagnostic te <u>3 years</u>	ed for each individ nents/component St) 4 years	is used in. See				
Beta Factor Verification Proof Test Interval PFD (avg.) (IEC 61508-6, B3.2.2; λ _{du} from fail Single component application (H	$\beta_{int} = 5\%$ $\beta_{Dint} = 2\%$ of SIL Capa (see contribution) (see c	calculation, b Beta factor, w architectures The beta fact IEC 61508-6, ability (ex ability (ex	which has to be c with a HFT ≥ 1.1 or depends on th table D.5 how to camples cc page/backside of 1 year	exact architecture calculate beta factor calculate beta factor calculate beta factor considering d this page) 2 years	has to be calculate where the compo or. iagnostic te 3 years 1.83 E-03	ed for each individ nents/component St) 4 years	is used in. See				
Beta Factor Verification Proof Test Interval PFD (avg.) (IEC 61508-6, B3.2.2; λ _{du} from fail Single component application (H Max. achievable SIL acc. IEC 61508-1, table 2 a Redundant component applicatio	$\beta_{int} = 5\%$ $\beta_{Dint} = 2\%$ of SIL Capa (see contribution) (see c	calculation, b Beta factor, w architectures The beta fact IEC 61508-6, ability (ex ability (ex 4.2, Route 1 _H 4.2, Route 1 _H 4.2, Route 1 _H	which has to be c with a HFT ≥ 1.1 or depends on th table D.5 how to camples cc page/backside of 1 year 6.13 E-04	exact architecture calculate beta factor calculate beta factor calculate beta factor considering d this page) 2 years	has to be calculate where the compo- iagnostic te 3 years 1.83 E-03 SIL 2 SIL 3	ed for each individ nents/component st) 4 years 2.44 E-03					
Beta Factor Verification Proof Test Interval PFD (avg.) (IEC 61508-6, B3.2.2; Adu from fail Single component application (H Max. achievable SIL acc. IEC 61508-1, table 2 a Redundant component application Max. achievable SIL acc. IEC 61508-1, table 2 a Calculated	βint = 5% βDint = 2% of SIL Capa (see com ure rates) IFT = 0) Ind IEC 61508-2, 7.4.4 INGENIEURBÜF Anzinger Str. 24	calculation, b Beta factor, w architectures The beta fact IEC 61508-6, ability (ex ability (ex 4.2, Route 1 _H 4.2, Route 1 _H 4.2, Route 1 _H	which has to be c with a HFT ≥ 1.1 or depends on th table D.5 how to camples cc page/backside of 1 year 6.13 E-04	onsidered if the con Detailed beta factor e exact architecture calculate beta fact onsidering d this page) 2 years 1.22 E-03	has to be calculate where the compo- iagnostic te 3 years 1.83 E-03 SIL 2 SIL 3	st) 4 years 2.44 E-03	is used in. Sec 5 years 3.05 E-0				

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Explanations to the Data Sheet						
The data sheet is divided in 4 areas:						
 Common technical description of the set of components/component (blue) Failure rates (light green) 	Common technical description of the set of components/component (blue) Failure rates (light green)					
 Specification of architecture of the set of components/component (light orange) Verification of SIL capability (examples) (grey) 						
General description of the Part / Component:						
 Information on the set of components/component, type of component and component designator Manufacturer information 						
 Component type (Type A or Type B) acc. IEC 61508-2/7.4.4.1.2 und 7.4.4.1.3) 						
 Mode of operation of the set of components/component (acc. IEC 61508-1) Description of the safety function of the set of components/component 						
Description of the safe state of the set of components/component						
Failure Rates and Failure Rate Distribution						
The failure rates and failure rate distribution are the results of the reliability calculation of the set of components/ component and the Failure Modes Effects and Diagnostic Analysis (FMEDA). The failure rates can be used for further quantitative analysis of the set of components/component as pfd/pfh-calculation, Markov-Analysis, Fault Tree Analysis, and due to this for a quantitative evaluation of SIL-capability of the set of components/component.						
Based on the failure rate distribution the Safe Failure Fraction (SFF) is calculated according the formula SFF [%] = $(\lambda_S + \lambda_{DD}) / (\lambda_S + \lambda_{DD} + \lambda_{DU})$.						
Specification of Component Architecture						
The architecture of the set of components/component is described by following parameters:						
 Structure/architecture (single-channel, multi-channel expressed by 1001, 1002, 1003, etc.) Hardware-Fault-Tolerance (HFT) (number of failures acceptable without dispatch on the safety function 	on of the set of					
components/component)						
	general, the MRT is application specific. The user is responsible to define realistic MRT for the specific application. The					
 Mean Time to Repair (MTTR): Mean time to repair the set of components/component in case of detect failure. MTTR is the sum of MRT and diagnosis test interval. 	cted dangerous					
 Diagnostic Coverage: The diagnostic coverage is resulting from the diagnostic test for the set of components/component in case of application of automatic diagnosis (e.g. partial stroke test). The diagnostic coverage is considered in the FMEDA and the quantitative results of the analysis (see failure rates). 						
 Diagnostic Test: The type of installed on-line automatic diagnostic test to detected dangerous failure diagnostic test has to fulfill requirements acc. IEC 61508-2. 	during operation. The					
 Diagnostic Test Interval: Interval between diagnostic tests to detect dangerous failures. Longer diagnostic test intervals as specified in the datasheet has to be considered separately in safety parameter calculations, see IEC 61508-2, 7.4.9.4. 						
 Beta Factor: If the components/component is used in safety relevant architecture with a HFT ≥ 1 a beta factor has to be considered in safety loop calculations. The beta factor for the component is initial (β_{int}). To estimate the final beta factor for a specific application the effects of the architecture have to be considered. Thus the beta factor has to be calculated individual according IEC 61508-6, table D.5. 						
 Beta Factor Diagnostics: β_D is the fraction of dangerous common cause failures if the components/component is used in safety relevant architectures, which can be detected by diagnostic tests. see IEC 61508-6, table B1. 						
Verification of SIL-capability (examples)						
The SIL verification consists of two steps:						
 Step (1) = quantitative verification by calculation of the pfd-value / pfh-value depending from the defined Proof Test Interval and used architecture. The max. reachable SIL for the calculated safety loop within the component is used can be 						
 estimated according IEC 61508-1 table 2 (for low demand operation) or table 3 (for high demand operation) Step (2) = qualitative verification based on the architectural information of the set of components/component 						
according route 1_{H} , the qualitative max. SIL is defined in IEC 61508-2, 7.4.4.2.2 Tab. 2. The final achievable SIL is the minimum resulting SIL-value of step (1) and step (2): MIN {(1); (2)}. The final achievable SIL is only relevant for the final safety loop not for a single component used in the safety loop.						
Further remarks using safety relevant parameters						
 If operating medium is required (oil, air, etc.), failure rate of operating medium is not considered in the safety related 						
 parameter shown in this datasheet. Failure Rates considering diagnostic measures with DC > 0 may only be used if diagnosis with sufficient quality is installed 						
in the application.						
 Common cause failures, which can occur using the analyzed component in architectures, have to be considered by the user in safety loop calculations. 						
 If the subsystem is used in application with architectures, e.g. in a 1oo2 architecture, a beta-factor for the subsystem derived from βint acc. IEC 61508-6, table D.5 has to be considered in the safety loop calculation of the application. 						
B160307_V10_SIL-Datasheet_Polna_Control Valve_Type Serie Z3_Actuator Serie PIR	Seite 2 von 2					
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